

"From Textbook to Practice: Ca History of Failure and Repair of Underground Wastewater Vaul

NSTITUTE

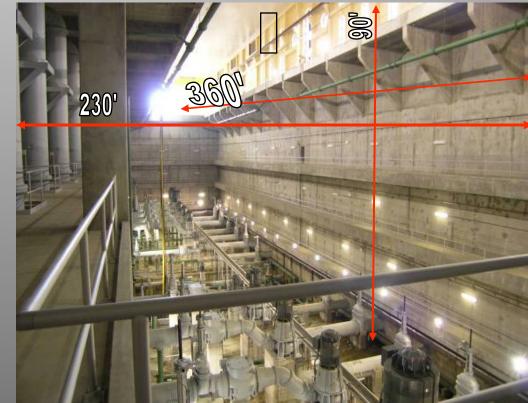
Prasad Samarajiva, Ph.D., P.E. Narendra Gosain, Ph.D., P.E. Gabriel A. Jimenez, Ph.D., P.E., S.E.

Structural Diagnostics Services Walter P Moore

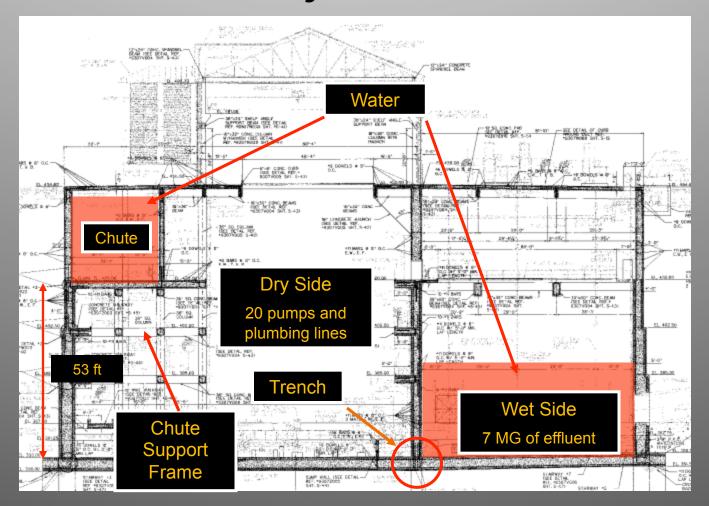
October 13, 2011

Size of wastewater vault

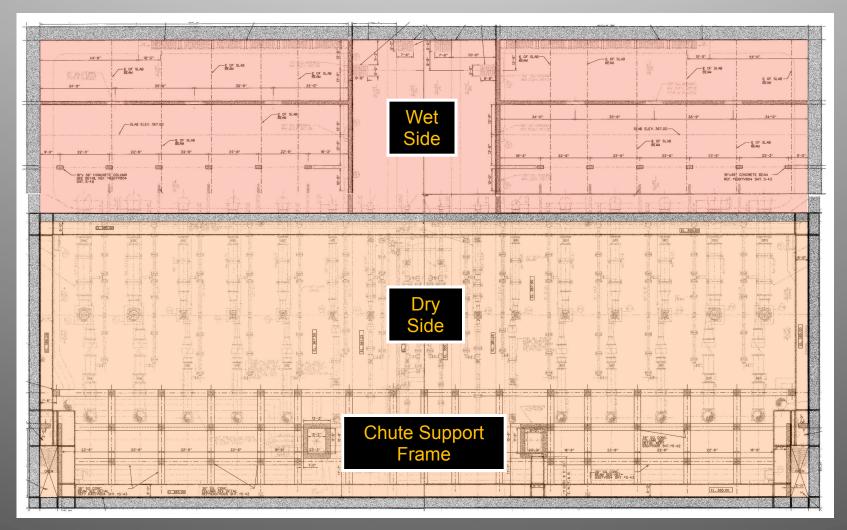
- 85 million gallons per day sewage treatment facility without pump station
- 600 million gallons per day with pump station
- Vault gross dimensions:
 - 230 ft. wide
 - 360 ft. long
 - 90 ft. deep
- Constructed using open excavation in limestone
 - Approximate side slope of 45 degrees



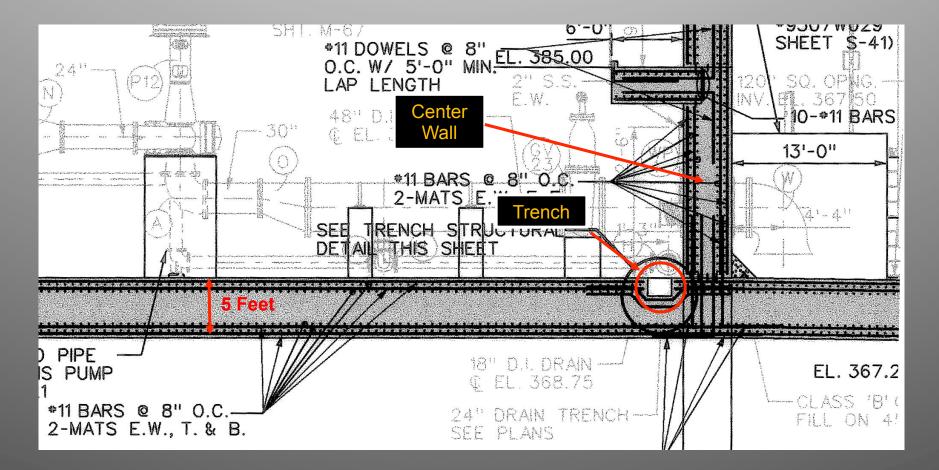
As-Designed Vault Section: major functional areas



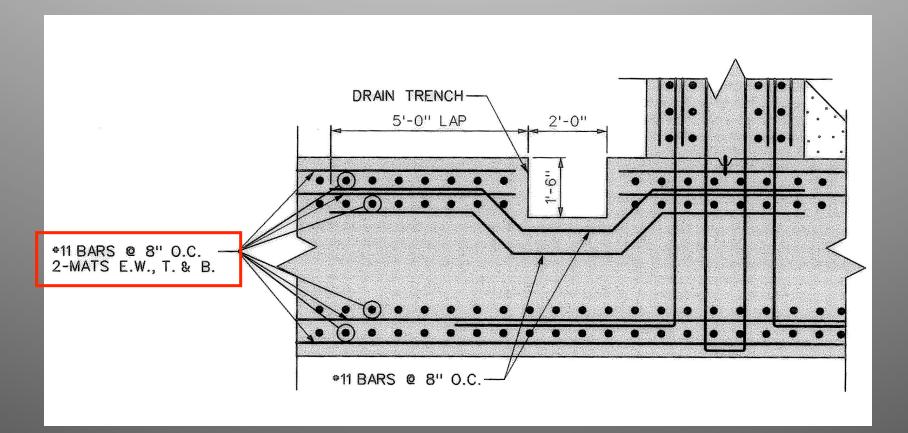
As-Designed Vault Plan



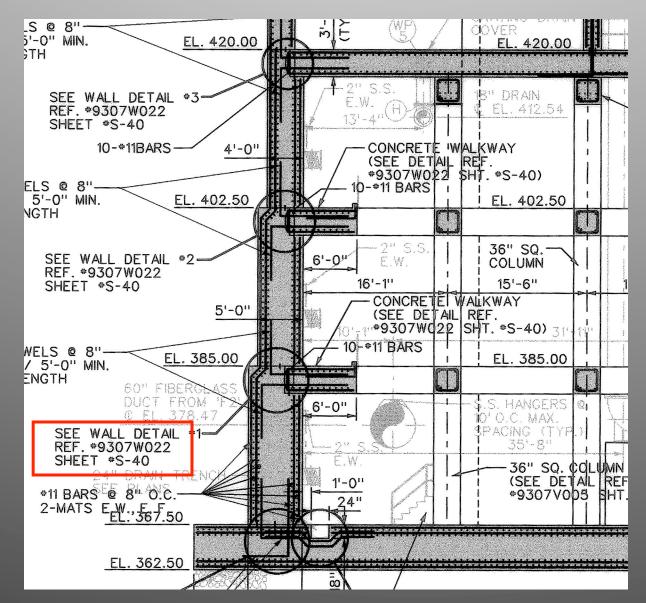
As-Designed Mat Slab



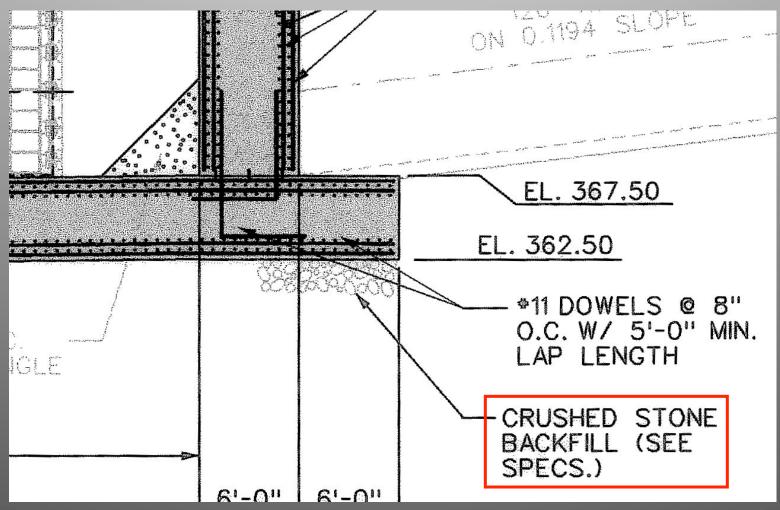
As-Designed Trench at Interior Wall



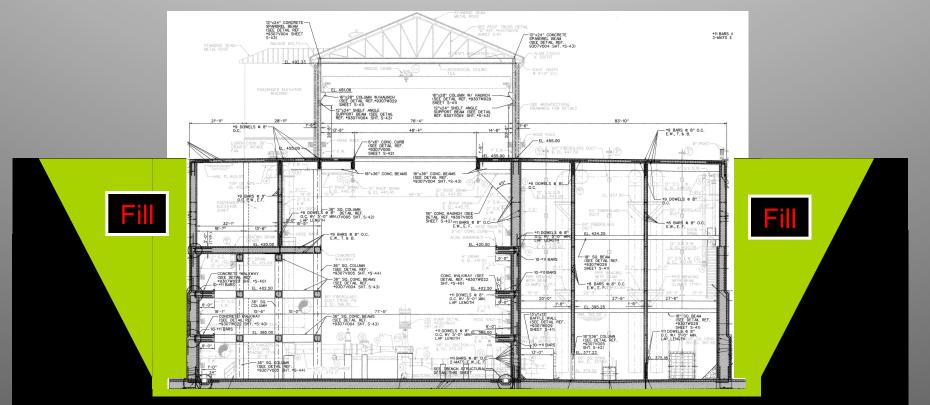
As-Designed Wall Section(Typical)



As-Designed Backfill Under Mat Slab



As-Built Location of Backfill





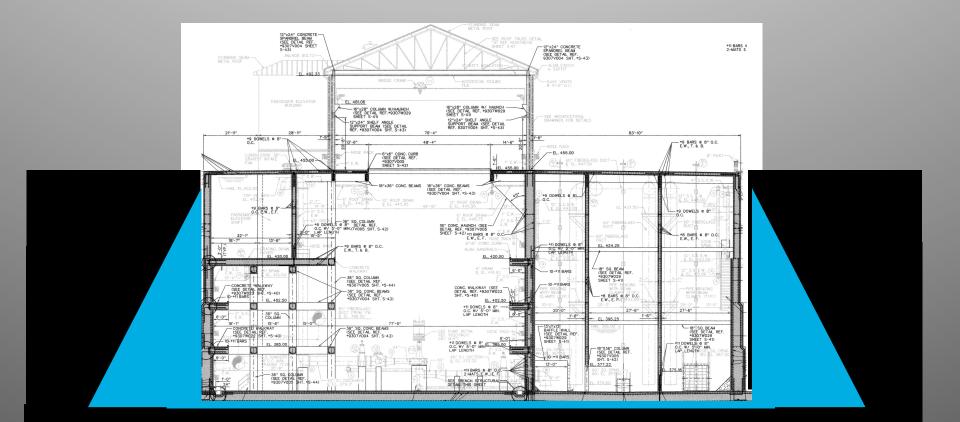
Geotechnical Design Considerations

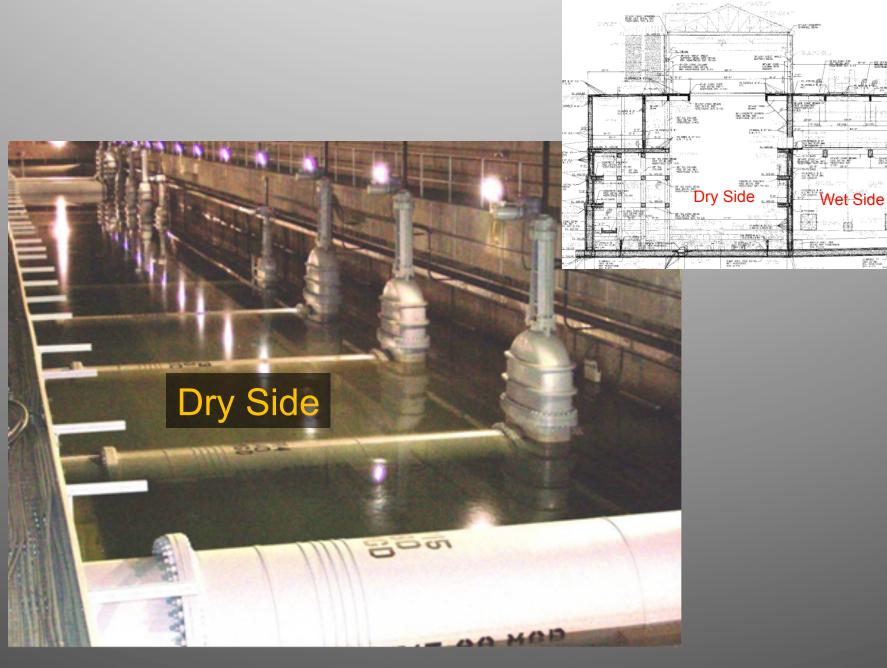
- Recommendations by Geotechnical Engineer
 - Wall backfill to be free-draining granular material.
 - Weep holes or foundation drains for walls required.
- Design parameters for walls by Geotechnical Engineer
 - Lateral earth pressure loads based only on fully drained conditions
 - Did not provide lateral design loads for saturated soil conditions.

Failure

- Heavy rains fell in the area days prior to the failure
- Failure occurred about three months after the vault was complete.
 - -Loud "popping" noises
 - Water flowed into the dry side of the vault reaching 15 ft above the base of the mat
- Vault was evacuated
- Groundwater level outside the pump station 2 days after the failure was 70 feet above the base of the mat.

Failure





State of the second second

rei

SLAPPER 17 Hat Etta ALL 434 Your

A HIERON

Groundwater flooded the dry side of the vault.

Post Failure Dewatering

- Dewatering wells were installed at the perimeter of the vault immediately after the failure.
- Groundwater level four days after the failure was found to be 70 feet above the base of the mat slab in this 90 feet deep vault.
- Continued dewatering removed millions of gallons of groundwater.
- Ground water was suspected to be coming from the nearby creek. However, no ground water infiltrations were observed during construction.

Possible modes of failures associated with loud "popping" sound

- Shear failure?
- Tension failure?
- Bending or flexural failure?
- Compression failure?
- Excessive cracking for sure!

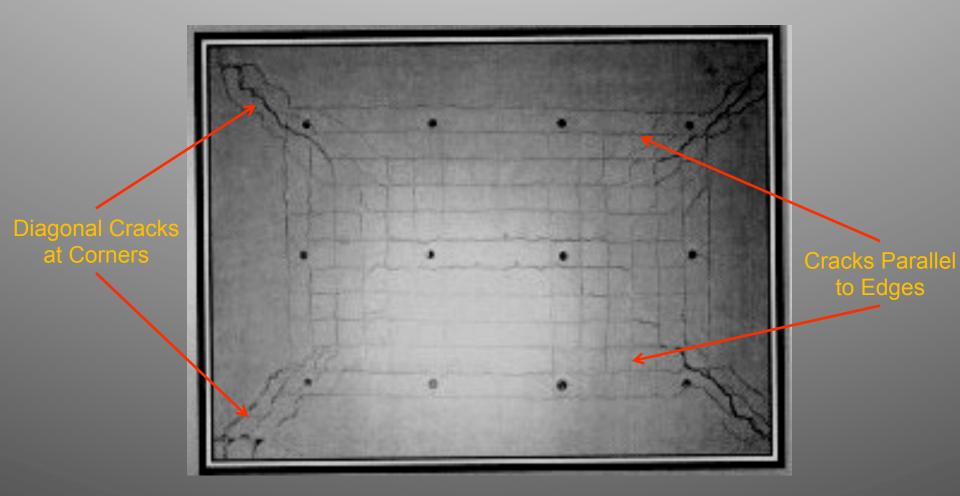
Field Investigation

- Damage Survey
 - -Mat slab
 - -Chute
 - -Chute support structure
 - -Perimeter walls
 - -Interior walls (Not covered in this presentation)
 - -Superstructure (Not covered in this presentation)
- Floor Level Survey

Damage Survey Slab Cracks

- Slab cracks noted in top face of slab.
- Crack patterns consistent with yield line pattern seen in uniformly loaded slabs.
 - -Diagonal cracks at corners.
 - -Cracks parallel to edges in middle.

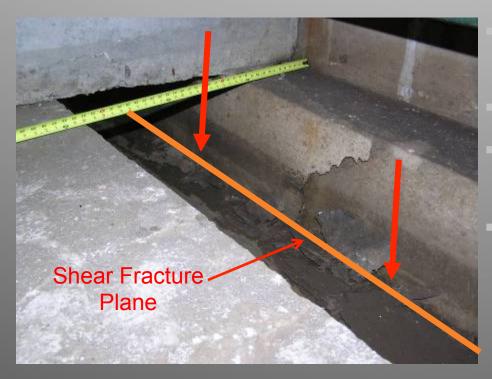
Classical Text Book Example Rectangular Slab Failure Pattern



Damage Survey Slab Cracking (Flexural Failure)

Yield Line Flexural Failure in Slab in Dry Side (Compare with text book example)

Damage Survey Fracture at Interior Trench

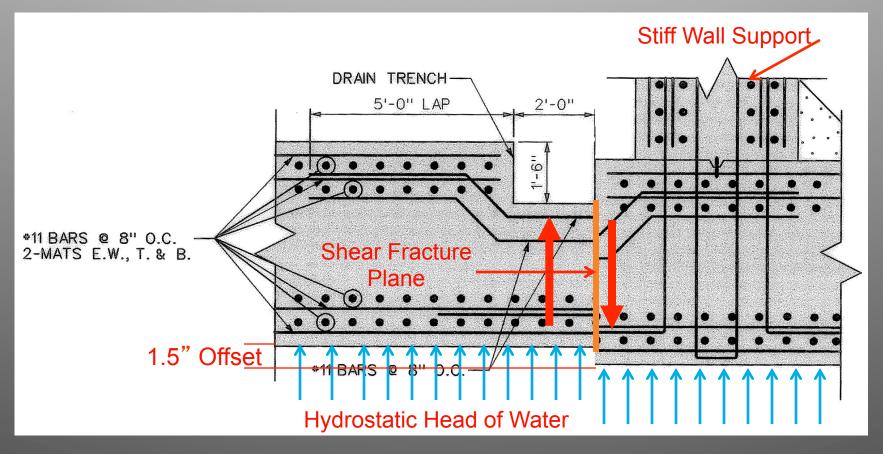


Mat slab fractured at trench.

Shear failure

- 1.5" floor level difference across fracture plane.
- Probable yielding of reinforcing at fracture plane.

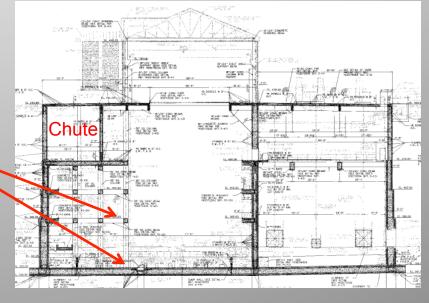
Damage Survey Fracture at Interior Trench



Shear Failure at Reduced (Weak) Section

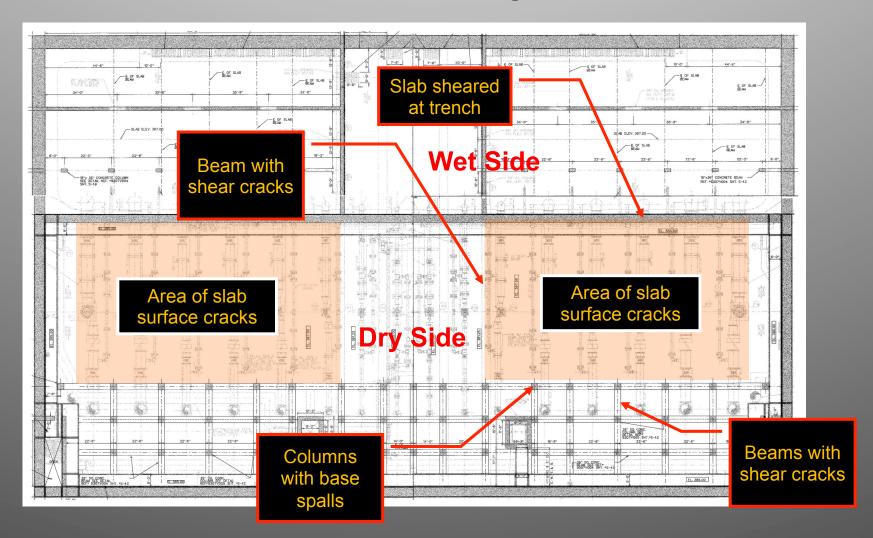
Damage Survey Chute Support Frame





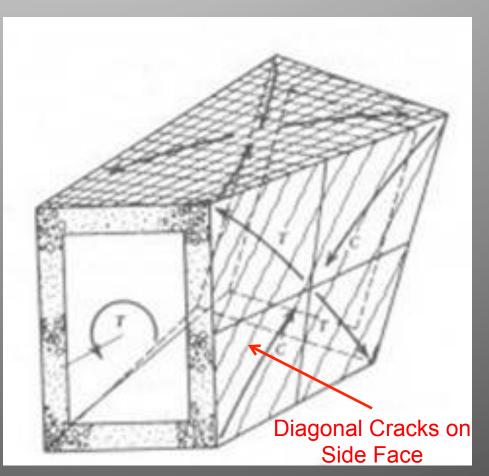
- Observations on 3' x3' Beams and Columns supporting Chute.
 - Spalls at base of columns.
 - Shear cracks in beams perpendicular to chute axis.
 - Crack widths ranged from hairline to more than 2".

Damage Survey Locations of Noted Damage



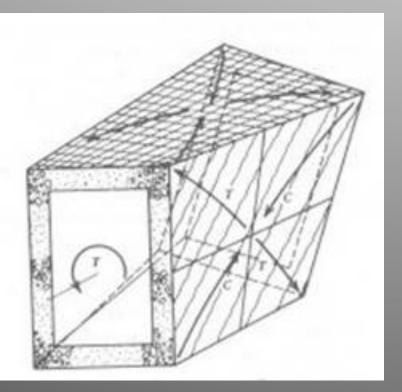
Damage Survey Torsional Cracking of Chute

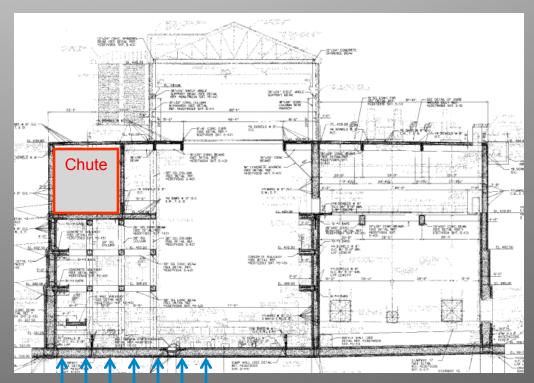
- Chute is a hollow square section measuring 35' X
 35'.
- Diagonal cracks found on sides and bottom at both ends (points of restraint).
- Crack patterns similar to torsion cracking of a hollow tube.



Text Book Example of Torsional Cracking of Hollow Tube

Damage Survey Torsional Cracking of Hollow Tube and Chute





Text Book Example of Hollow Tube Subjected to Torsional Force

Chute in Vault Subjected to Torsion Due to Upward Force in Mat Slab on Chute Support Frame

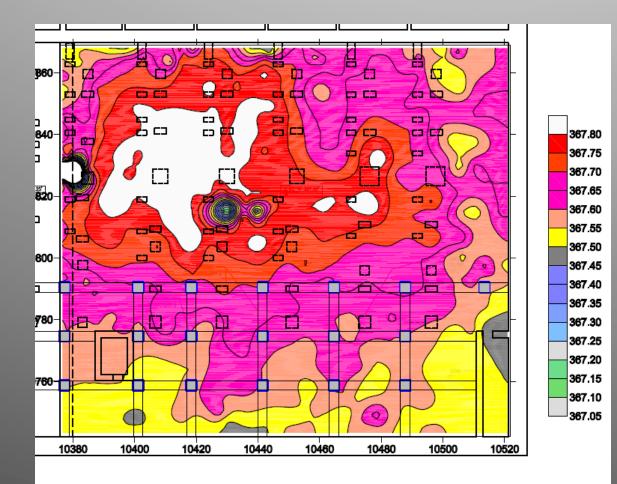
Damage Survey Torsion Cracking of Chute Side Wall



Damage Survey Torsion Cracking of Chute Bottom Face

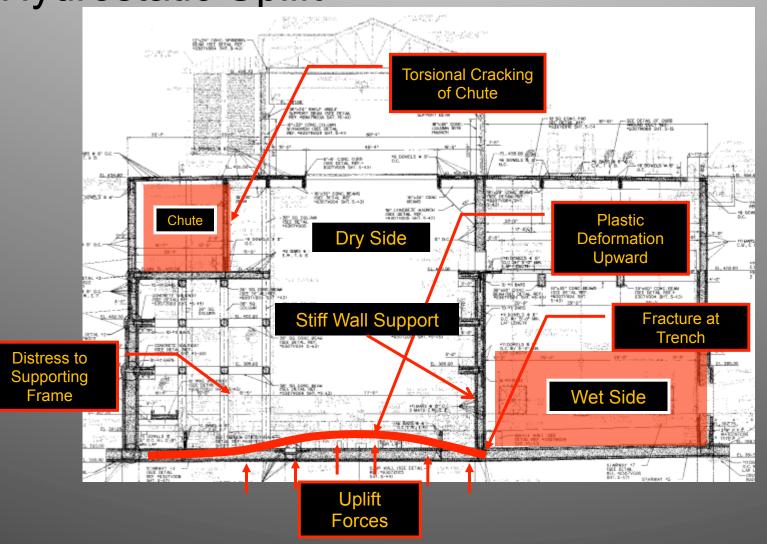


Field Investigation Floor Level Survey



4"-6" of floor level variations from reference floor level. 1"-2" permanent heave on dry side.

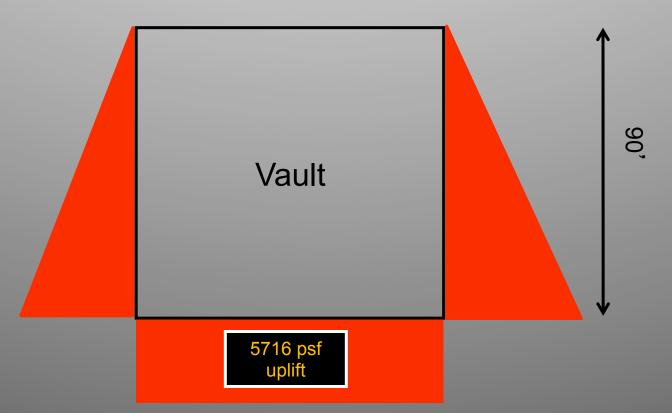
Failure Mechanism Based on Field Observations Hydrostatic Uplift



Geotechnical Investigation

- Sinkhole investigation (Not covered in this presentation)
- Groundwater study
- Evaluation of lateral earth loads
- Evaluation of uplift resistance

Geotechnical Investigation Groundwater Study

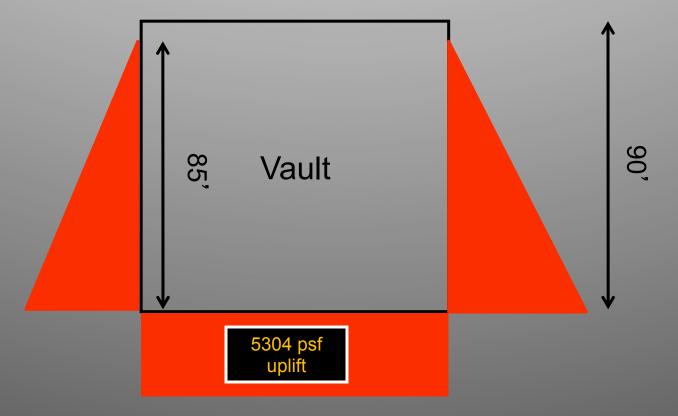


Forensic study – Recommend design condition for base mat slab under hydrostatic loads from groundwater

Groundwater Elevation at Time of Failure

- Groundwater level four days after the failure: 70 feet above the base of the mat slab.
- Groundwater elevation at time of failure: 85 feet above base of mat slab
 - Estimate based on the following
 - Flow of volume of water into vault
 - Porosity of backfill

Groundwater Elevation at Time of Failure



Geotechnical Investigation -Lateral Loads: Earth plus Water

- Original GEOR provided design lateral loads for earth pressure only (not saturated conditions), assuming fully drained backfill: 45 pcf.
- Forensic analysis determined design lateral loads for fully saturated conditions: 82 pcf

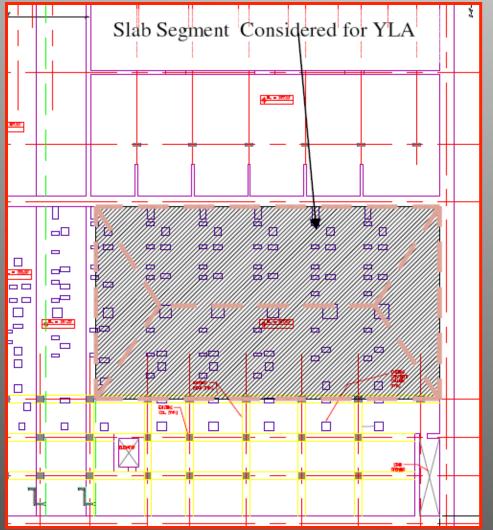
Structural Design Review

- Review of Engineer of Record design calculations
- Only 4 pages of engineering calculations found for perimeter walls
 - -Other calculations "lost"
 - -Serious errors in calculations in all 4 pages

Structural Design Review

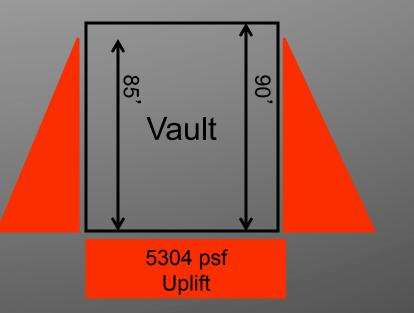
- Slab failure analysis
 - -Yield line analysis
 - -Finite Element Analysis
- Global structural design review
 - -Finite Element Analysis
 - -Hand calculations (sanity check)
- Uplift analysis.

Design Review Yield Line Analysis

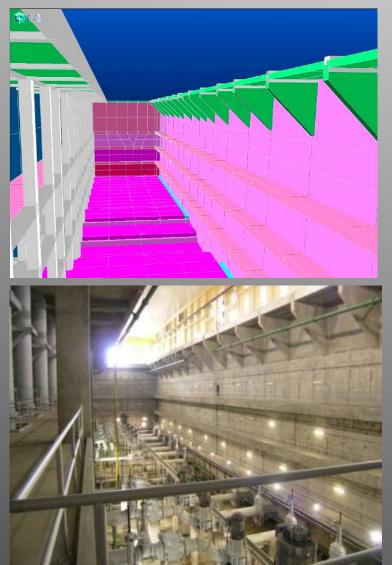


Failure Load

- Calculated failure load of slab: Hydrostatic uplift from ground water 2' below ground surface.
- Estimated groundwater elevation at time of failure: 5' below ground surface.



Design Review -Finite Element Analysis

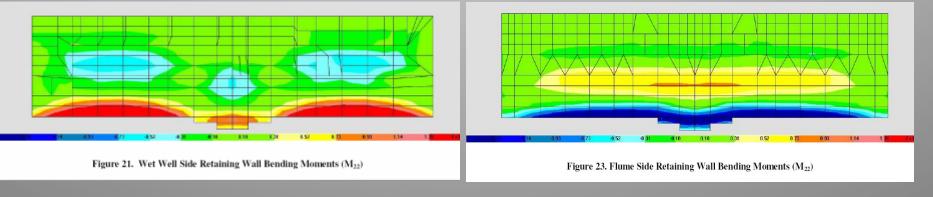


- 3-D Finite Element Analysis of entire vault.
- Detailed model considering all structural elements.
- Linear elastic model.
- Considered load cases:
 - Design
 - Failure

Design Review Finite Element Analysis Perimeter Wall Forces

Net Side

Dry (Chute) Side



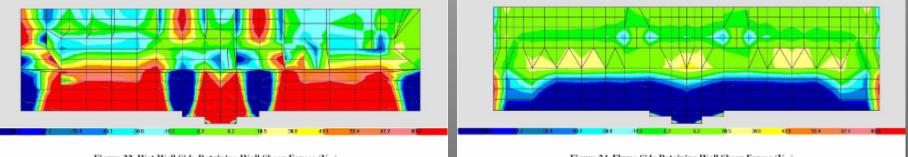


Figure 22. Wet Well Side Retaining Wall Shear Forces (V23)

Figure 24. Flume Side Retaining Wall Shear Forces (V23)

Forces exceed capacities in zones shaded in dark red and dark blue

Design Review Finite Element Analysis: Base Mat Slab

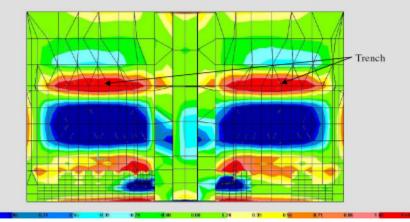


Figure 25. Mat slab Bending Moments (M22) In Design Loading Conditions

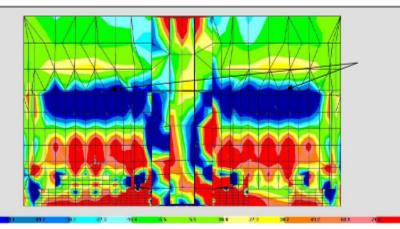
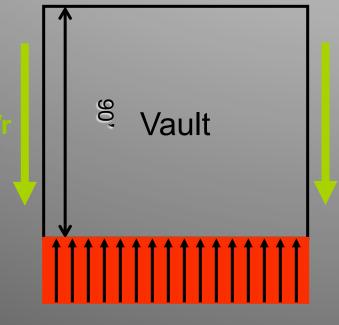


Figure 26. Mat slab Shear Force (V23) In Design Loading Conditions

Forces exceed capacities in zones shaded in dark red and dark blue Groundwater pressure was applied under the base mat

- Failure condition
 - -Along the trench
 - -Middle of the slab
 - -Under columns

Design Review Uplift Resistance



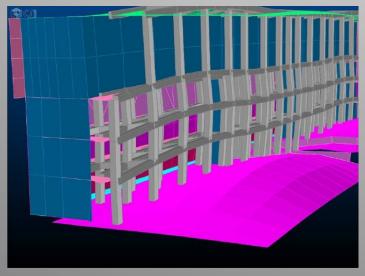
Hydrostatic Uplift Pressure As designed factor of safety against uplift = 0.5.
Acceptable design requirements = 1.5.
Analysis indicates vault would have floated out of the ground if the base mat had not failed.

-Failure relieved external water pressure.

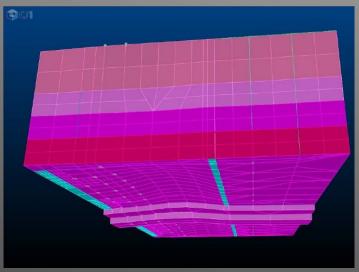
Design Review Conclusions and Recommendations

- Wastewater treatment vault not properly designed to resist applied design forces.
 - Perimeter Walls: Not designed adequately to resist shear from lateral earth pressures.
 - -Base Mat: Not properly designed to resist uplift forces from groundwater.
 - -Chute Support Frame: Not properly designed to accommodate lateral displacement of perimeter wall.
 - -Structure as a Whole: Not properly designed to resist uplift forces.

Failure Analysis Uplift from Hydrostatic Forces



Note Frame Racking and Chute Torsion



Groundwater pressure applied under the base mat.

- Analysis results:
 - -Slab heave
 - -Racking of frame
- -Torsion of chute
- Results very consistent with observed distress conditions.

Note Slab Heave

Failure Analysis FE Analysis/Base Mat Heave (Text Book Case)

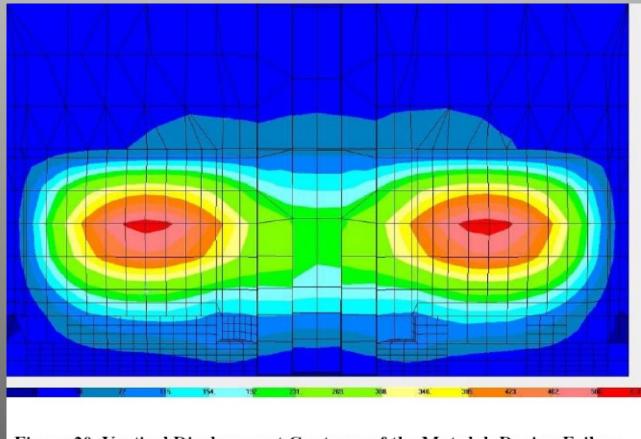
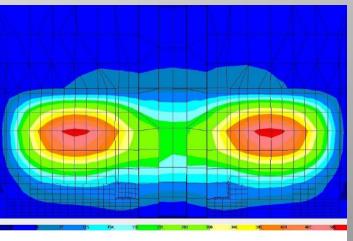
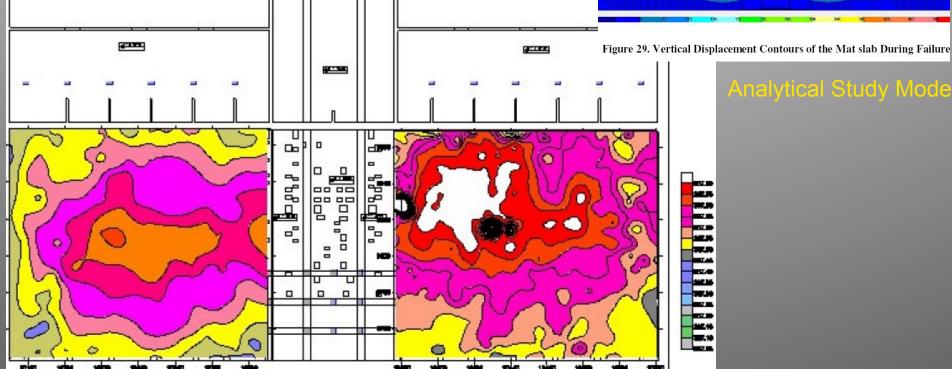


Figure 29. Vertical Displacement Contours of the Mat slab During Failure

Analytical Study Model

Failure Analysis Base Mat Slab





Analytical Study Model

Figure 30. Measured Heave Contours of the Mat slab (See Appendix A)

Base Mat Contour Survey

Failure Analysis Finite Element Analysis: Base Mat

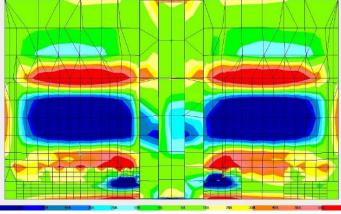


Figure 31. Mat slab Bending Moments $\left(M_{22}\right)$ In Failure Loading Conditions

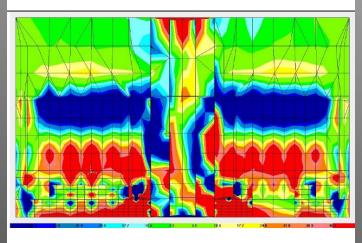


Figure 32. Mat slab Shear Force (V23) In Failure Loading Conditions

Forces exceed capacities in zones shaded in dark red and dark blue

Groundwater pressure was applied under the base mat

Locations of failure conditions are in general agreement with field observations.

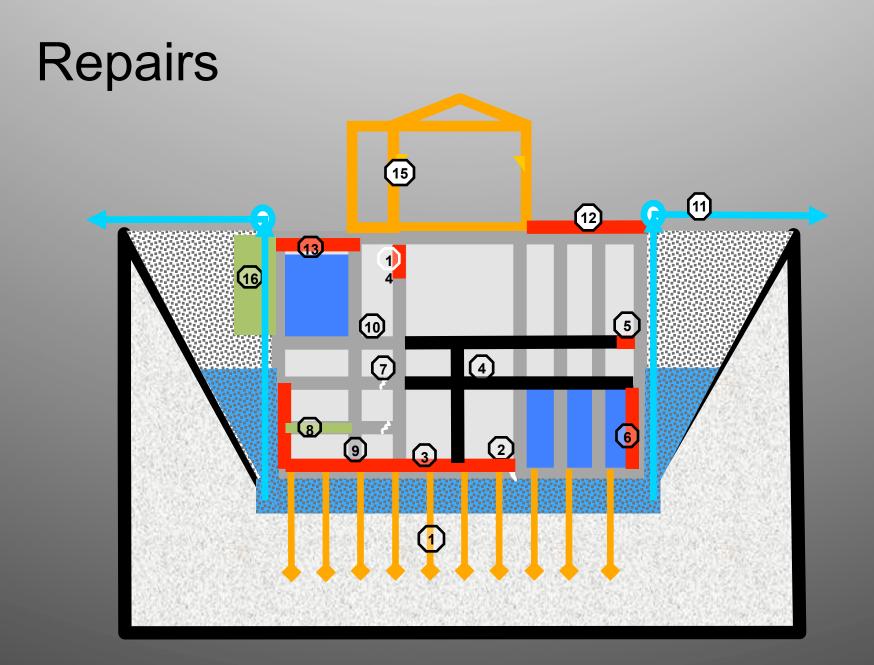
Failure Analysis Conclusions

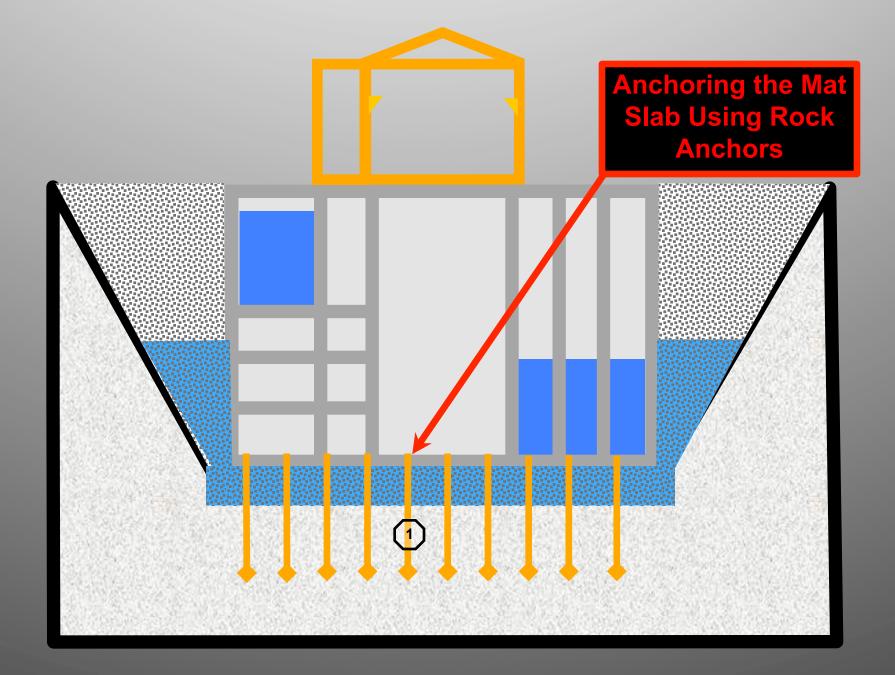
- Failure of the base mat: Due to uplift forces from groundwater.
- Groundwater elevation at time of failure: Near the ground surface.

Conclusions

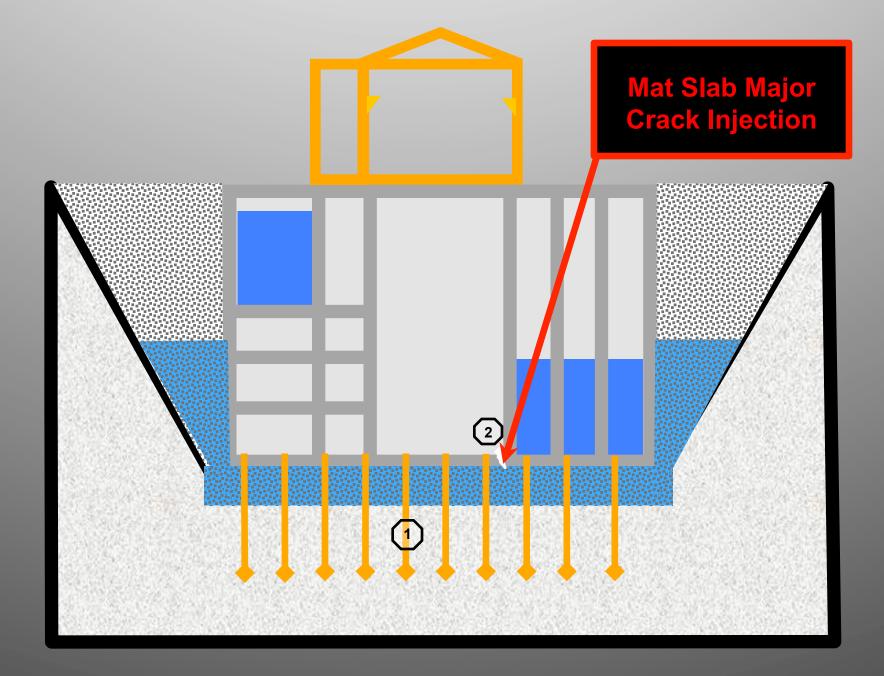
- Structure inadequately designed to resist:
 - -Lateral earth pressure
 - -Groundwater pressure on sides or bottom.
 - -Uplift forces.
- Structure failed
- Repair completed by April 2008

Some Repair Highlights

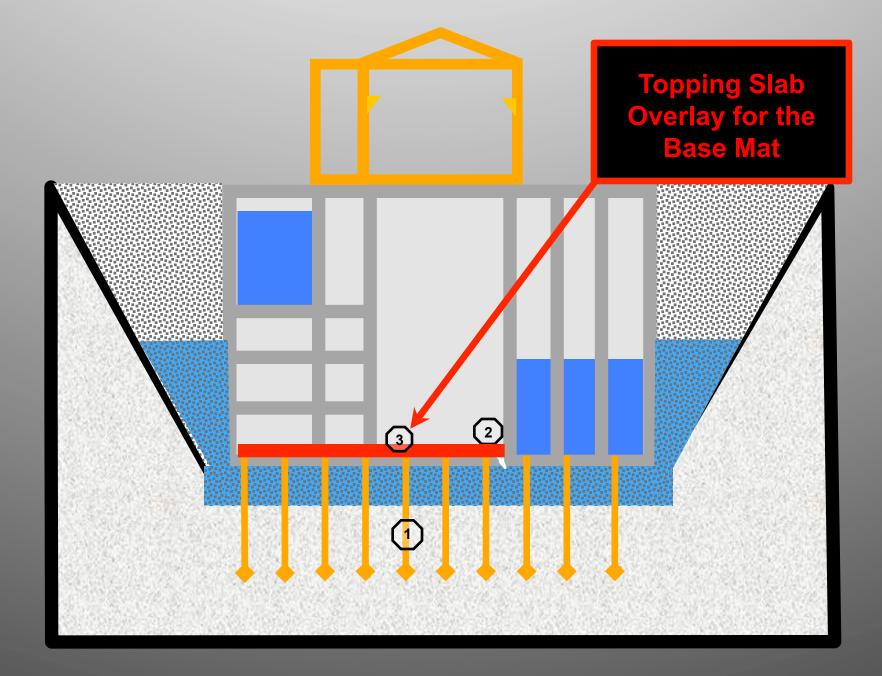




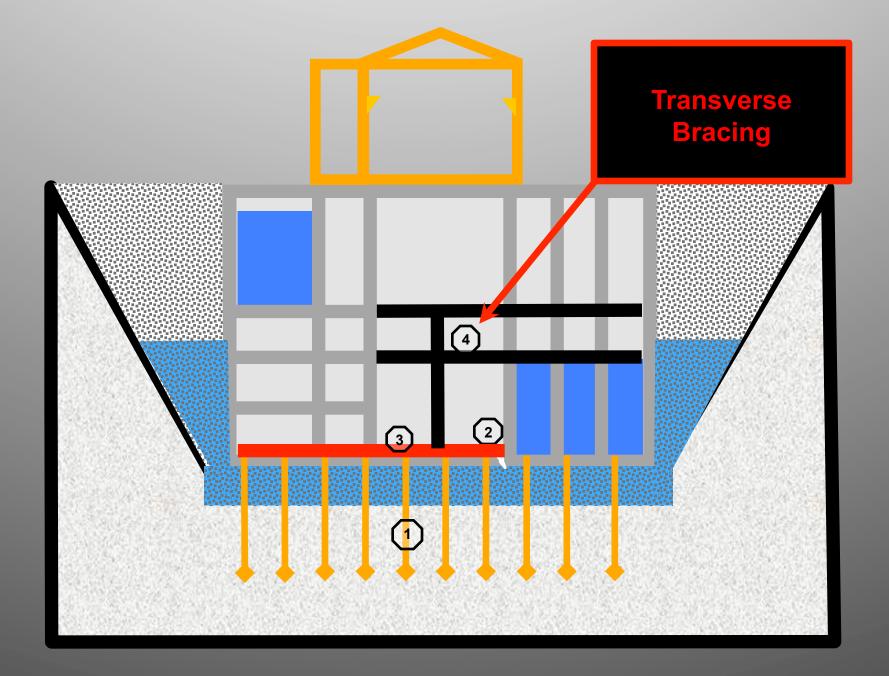




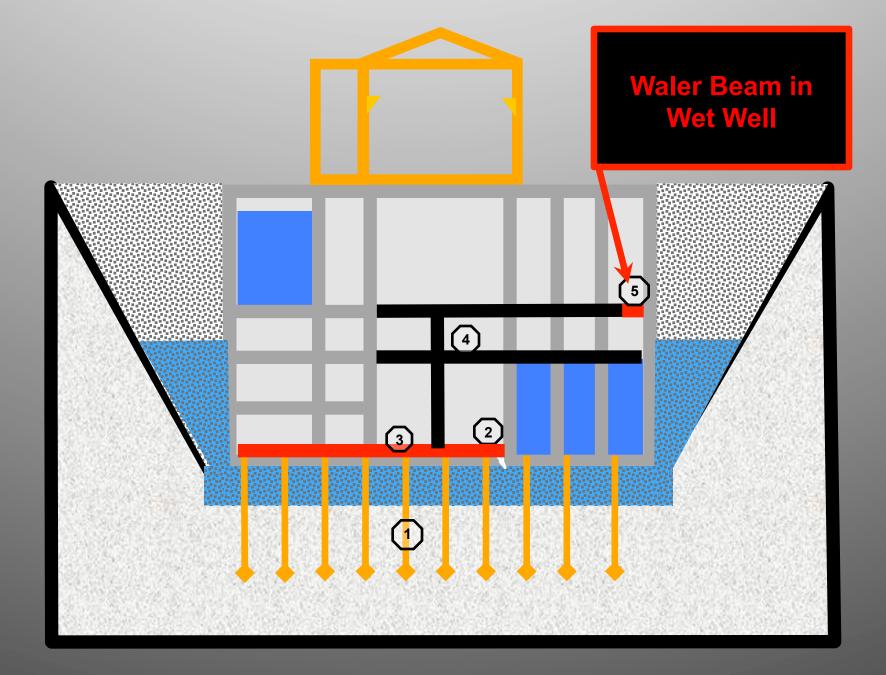




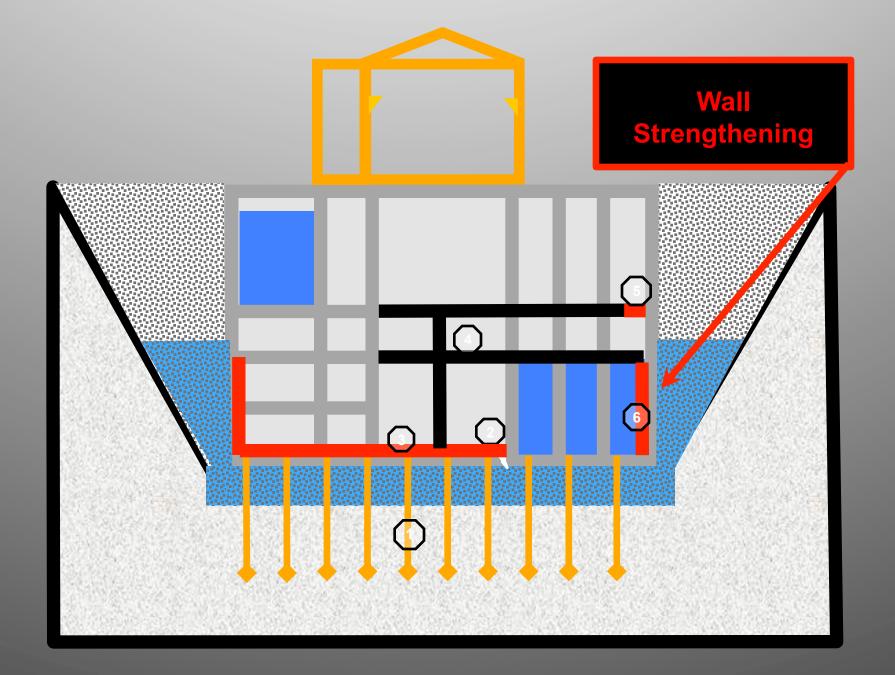




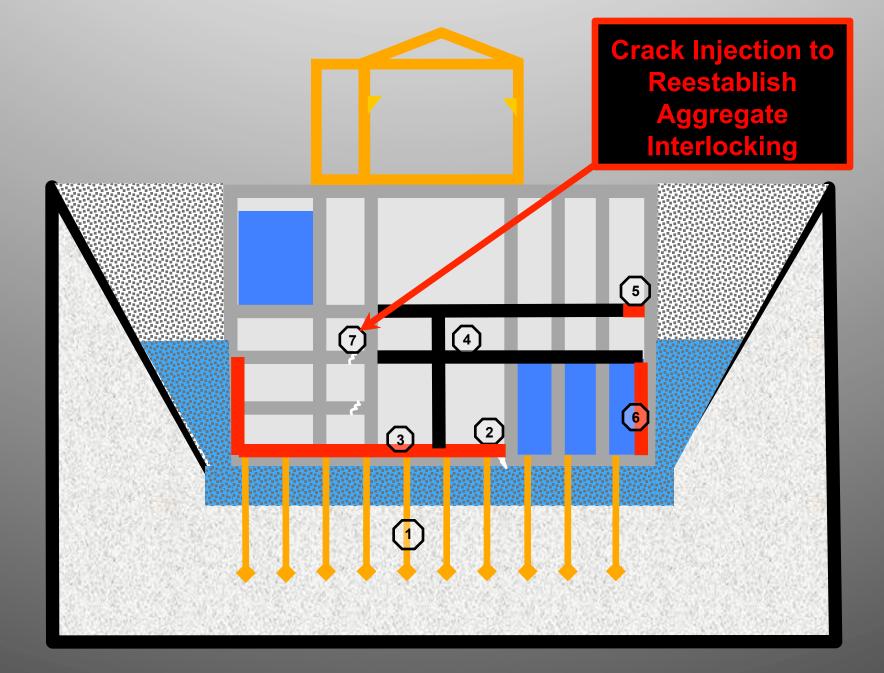


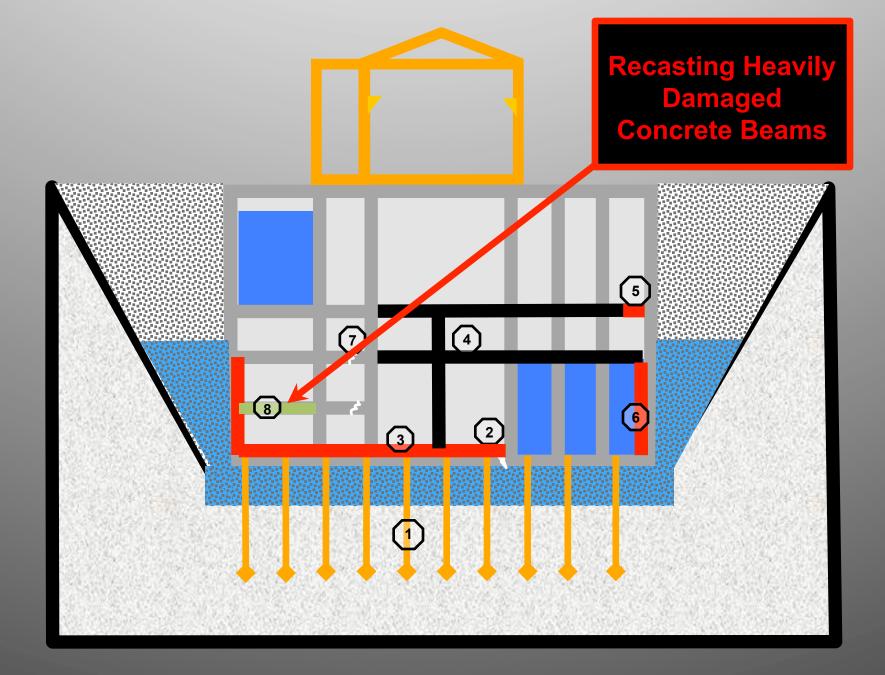




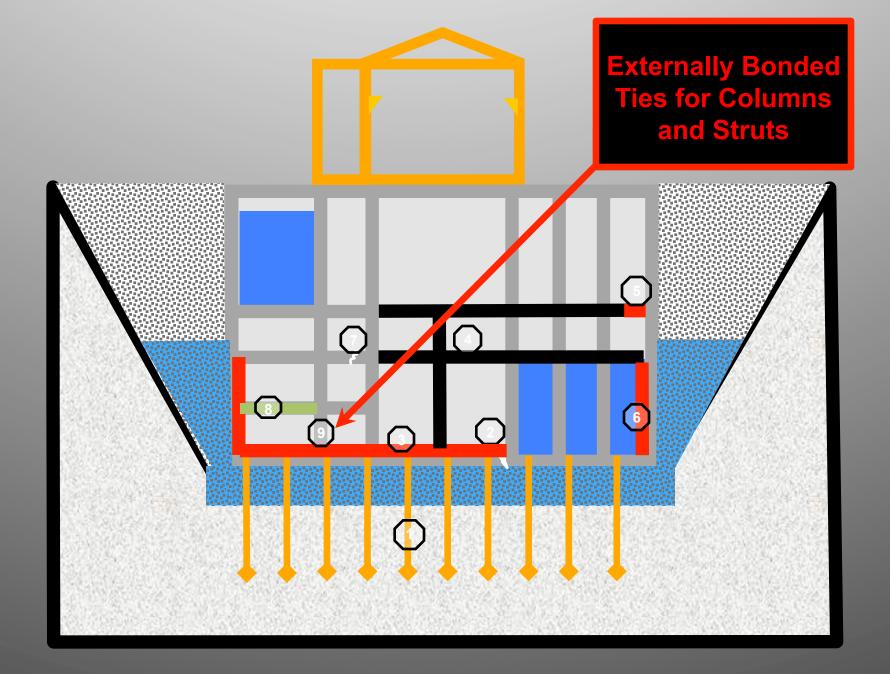




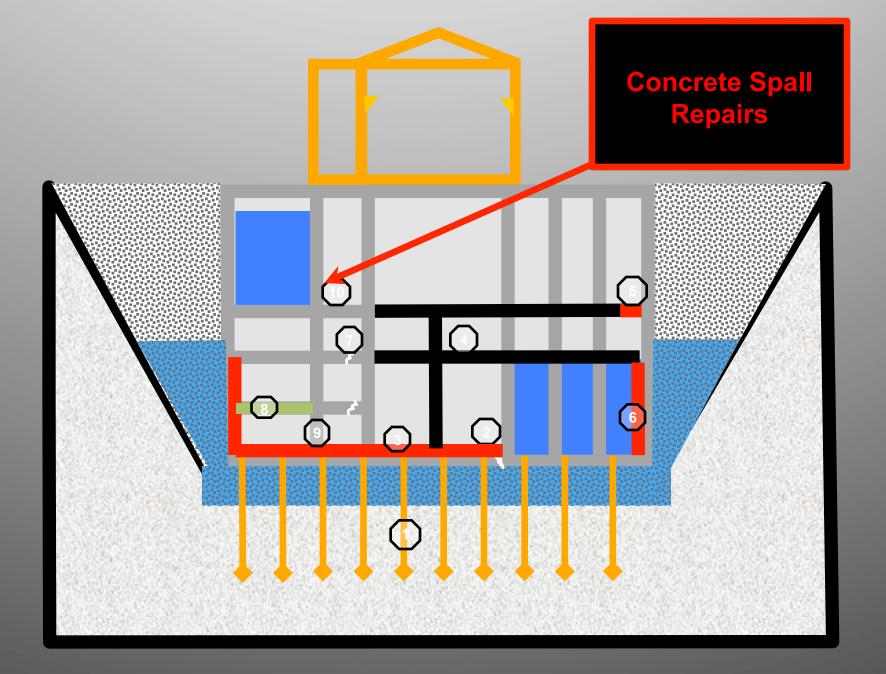


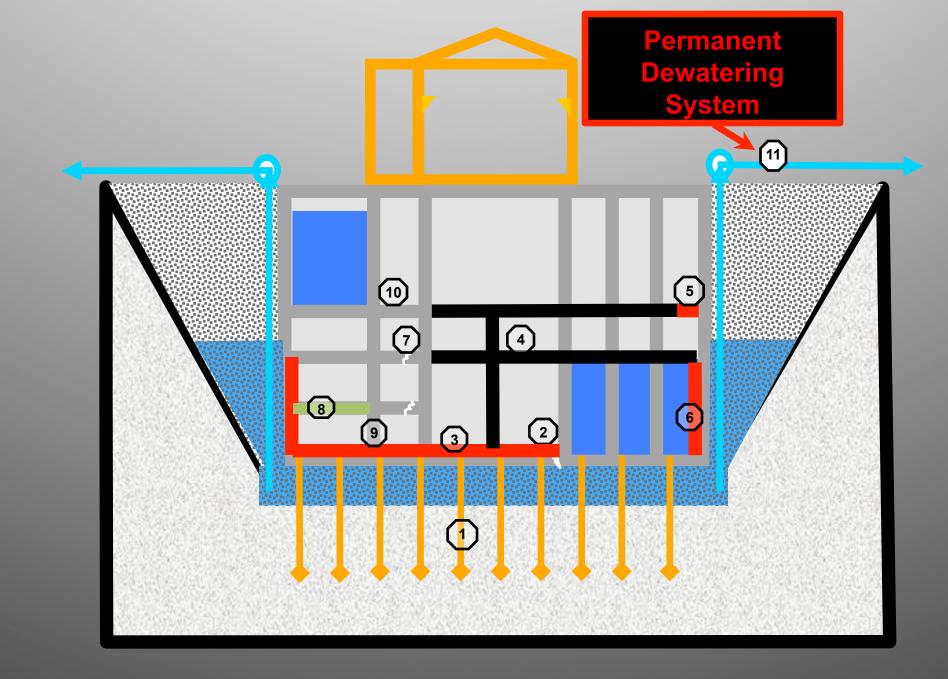




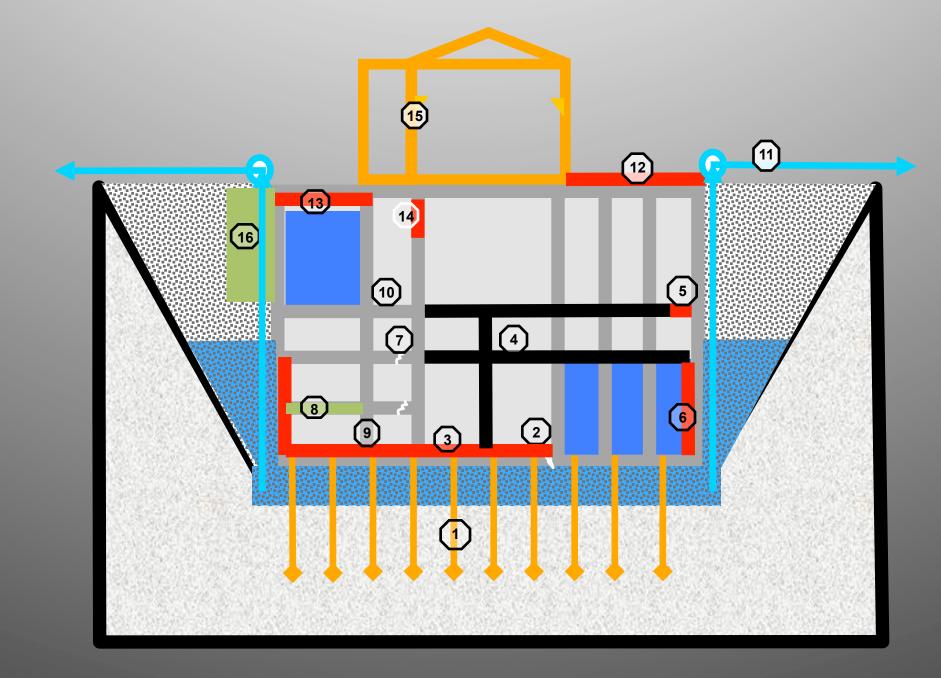












Questions?

NGosain@WalterPMoore.com PSamarajiva@WalterPMoore.com GJimenez@WalterPMoore.com

WALTER P MOORE Structural Diagnostics Services